

Integrated Modelling in JAEA



**TOPICS-IB: TOPICS extended to
Integrated simulation for Burning plasma
- Integrated modeling of transport and MHD -**

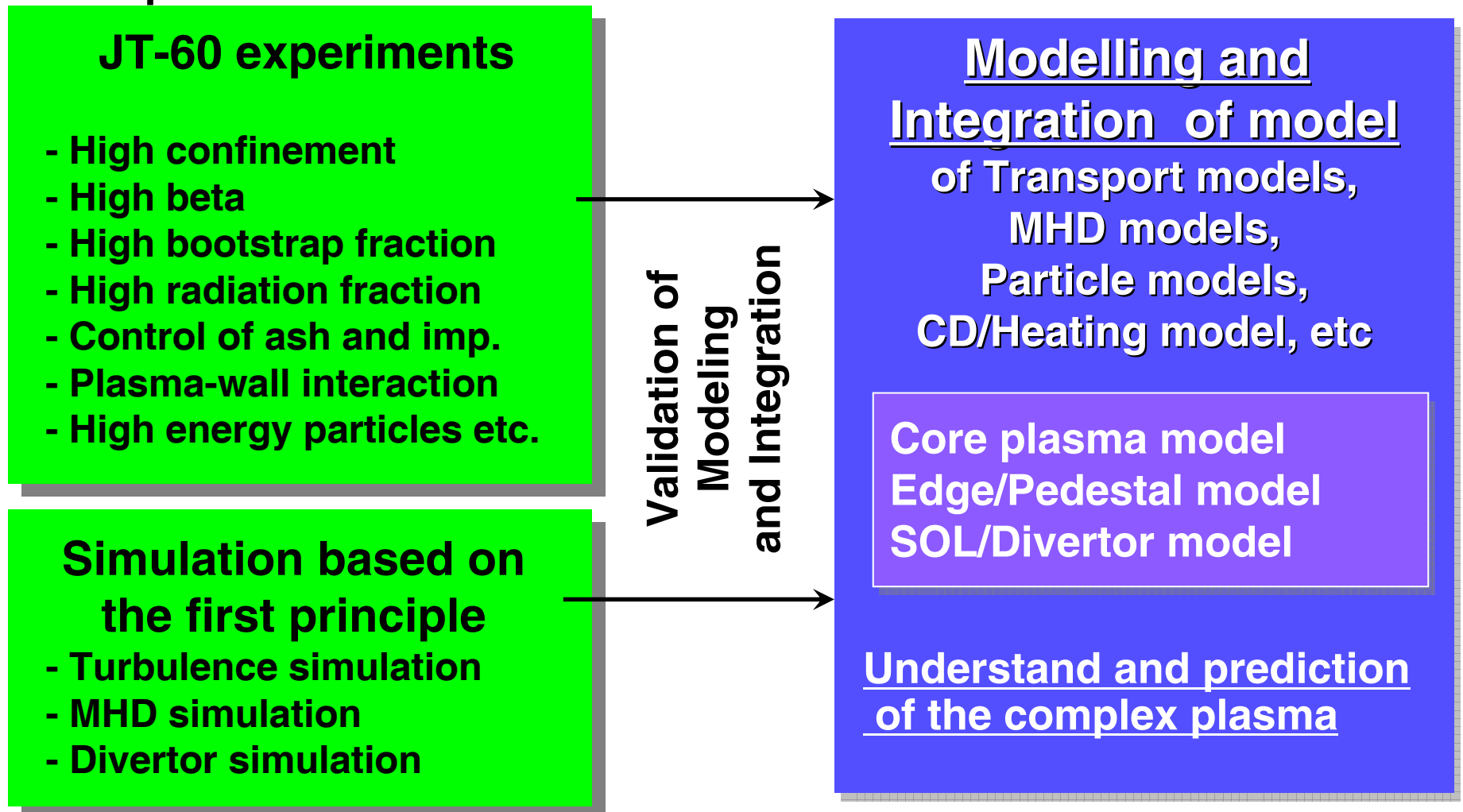
**Presented by T.Ozeki
Japan Atomic Energy Agency**

**US/Japan JIFT workshop on Integrated simulation of fusion plasmas
Jan.29-Jan.31, 2007 ORNL**

Strategy of Modelling / Integration of model

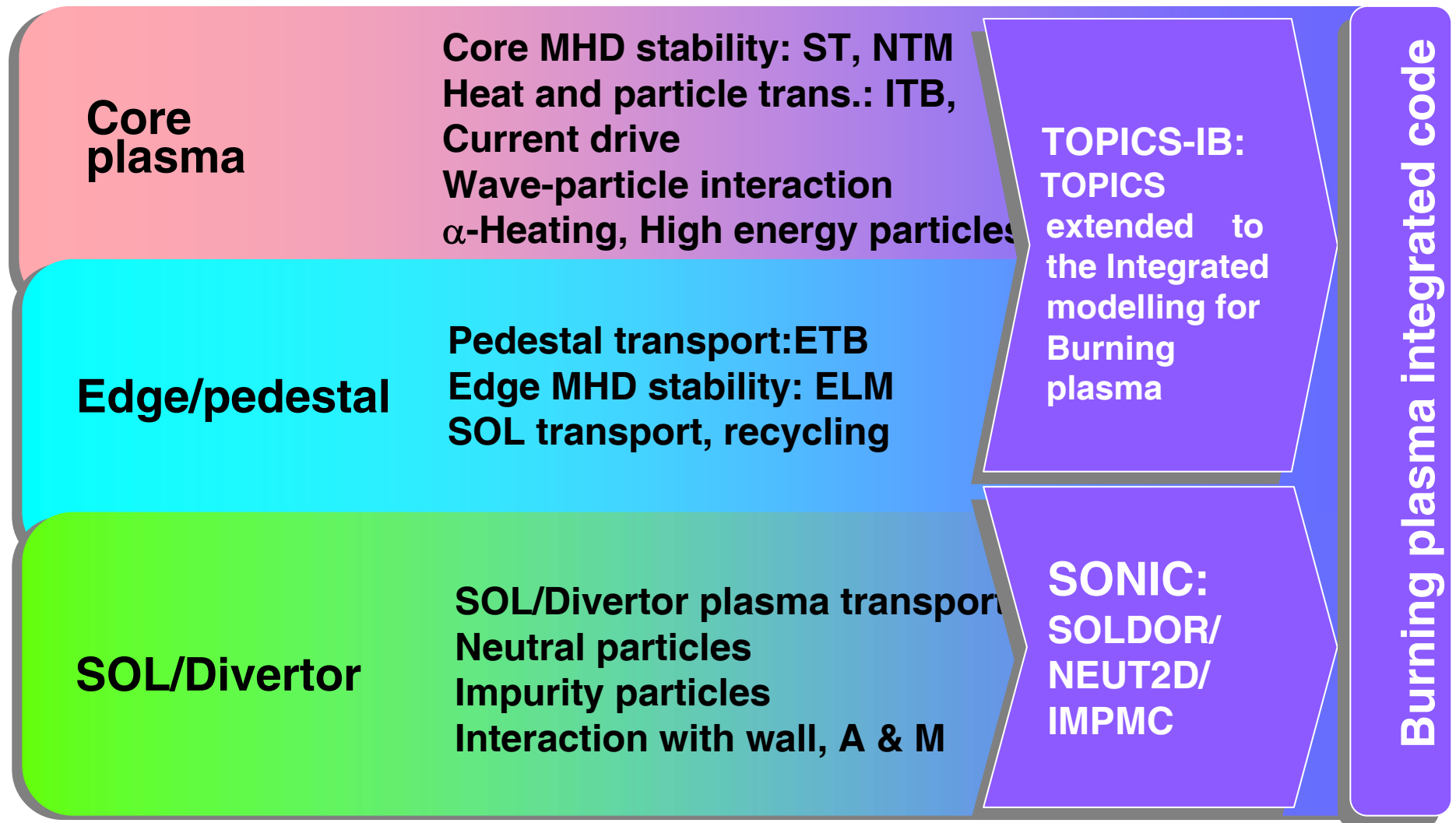
Integrated modelling in JAEA

Purpose is to understand and control the burning plasma which has the complexity and autonomy. Modeling and integration of model are developed based on the fundamental researches.



Development of integrated models

Integrated modelling in JAEA



TOPICS-IB: TOPICS extended to Integrated simulation for Burning plasma

Integrated modelling in JAEA

Transport code TOPICS

Tokamak Production and Interpretation Code
1D transport and 2D equilibrium, Matrix Inversion Method for NeoClassical Trans.

Transport

Transport model in core plasma

Heating, Current Drive

ECCD/ECH (Ray tracing, Relativistic F-P), NBCD(1 or 2D Fokker-Planck)

Neutral and α particles

Orbit following monte carlo, F-P, Stix

Impurity Transport

1D transport for each impurities,
Radiation: IMPACT

MHD

Tearing/NTM, High-n ballooning,
Low and Mid.-n MARG2D

Pedestal-SOL-Divertor

Transport in pdestal/SOL/Divertor
ELM, Neutral, impurity

Integrated Modelling in JAEA



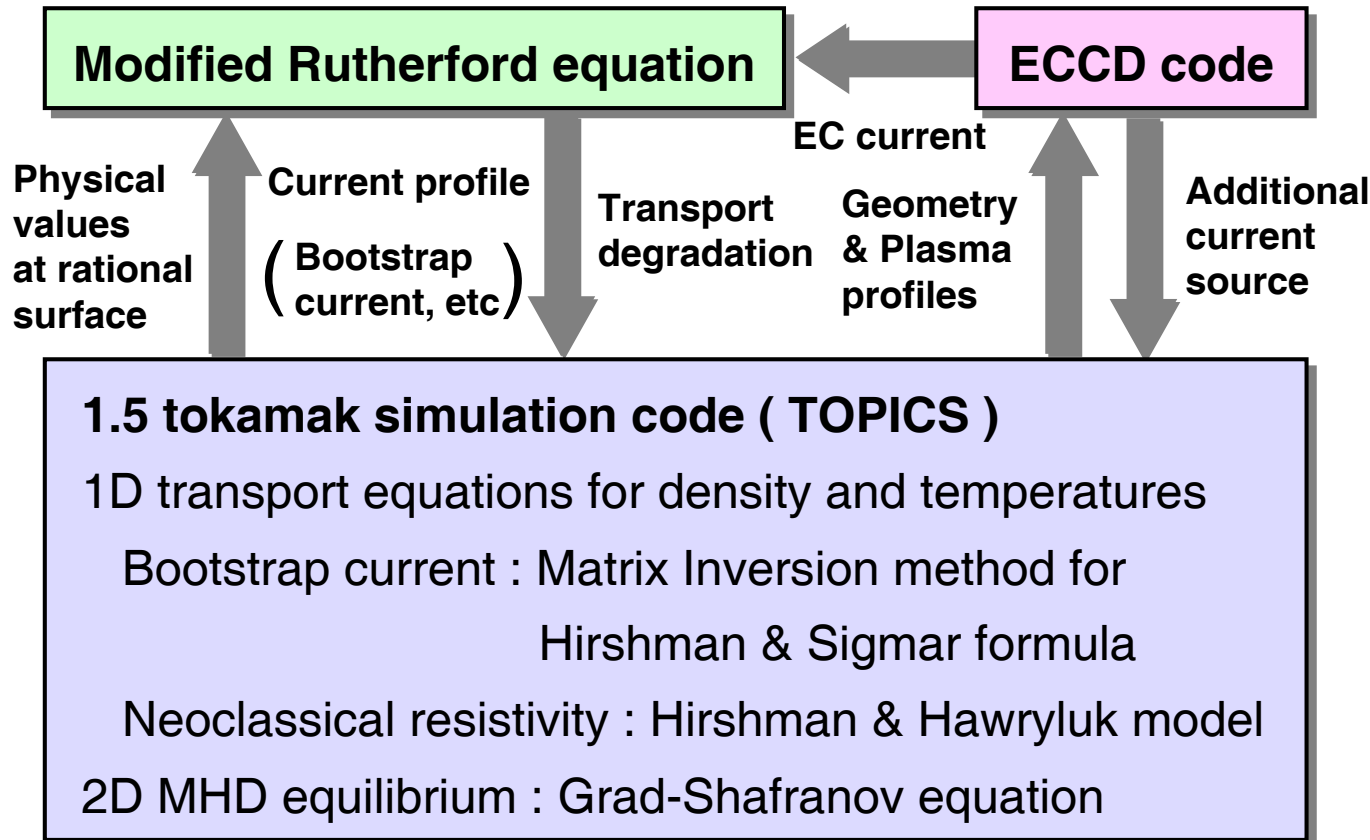
Integrated NTM model

mainly with A.Isayama, N.Hayashi

NTM simulation by Integrated model

Integrated modelling in JAEA

- **Neoclassical tearing mode (NTM)** are important to access and to sustain high β and it relates to the transport and MHD.
- For the stabilization of NTM, profile control and ECCD injection were demonstrated in JT-60U.



- To do the self-consistent analysis of stabilizing effect, 1.5D transport code, Modified Rutherford equation and ECCD code are integrated.

NTM model: Modified Rutherford equation

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$$\frac{\mu_0 a^2}{\eta} \frac{dW}{dt} = \Gamma_{\Delta'} + \Gamma_{BS} + \Gamma_{GGJ} + \Gamma_{pol} + \Gamma_{ECCD}$$

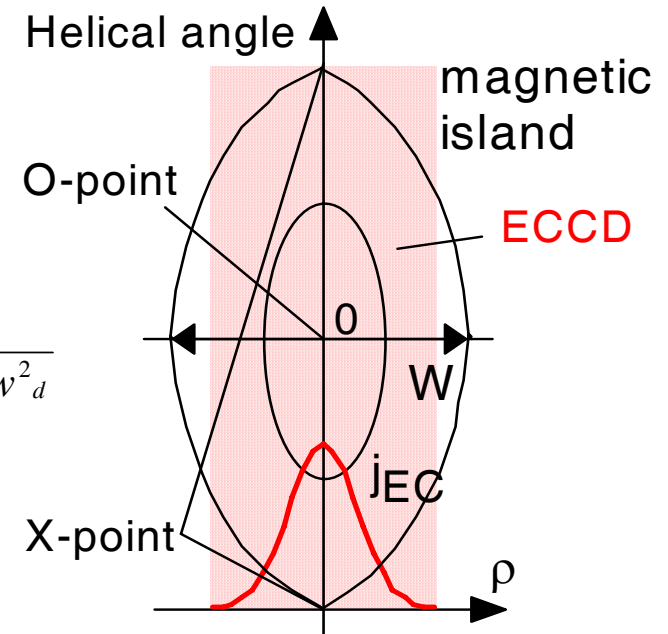
$\Gamma_{\Delta'}$: Classical tearing stability index term

Γ_{BS} : Destabilization by the lack of the bootstrap current due to plasma profiles flattened in the magnetic island.

Γ_{GGJ} : Stabilization by magnetic well (Glasser-Green-Johnson effect) $\Gamma_{BS} = k_3 \mu_0 L_q j_{BS} \langle |\nabla \rho| / B_p \rangle \frac{w}{w^2 + w_d^2}$

Γ_{pol} : Stabilization or destabilization by ion polarization current

Γ_{ECCD} : Stabilization by EC current compensating bootstrap current lost in the magnetic island.



χ : Diffusivities D_i, χ_e, χ_i

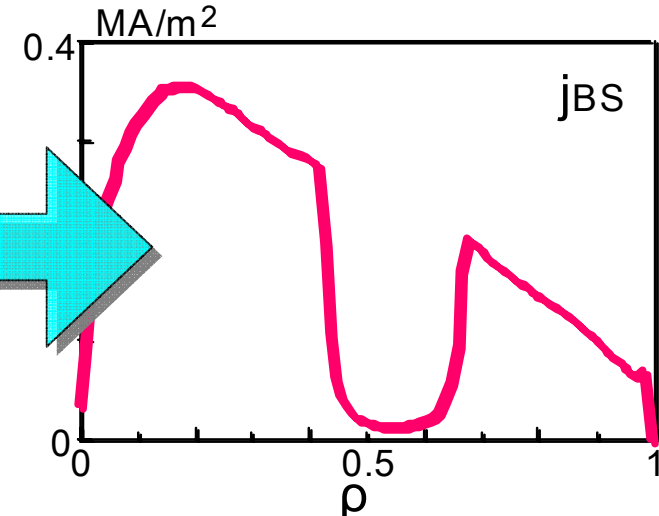
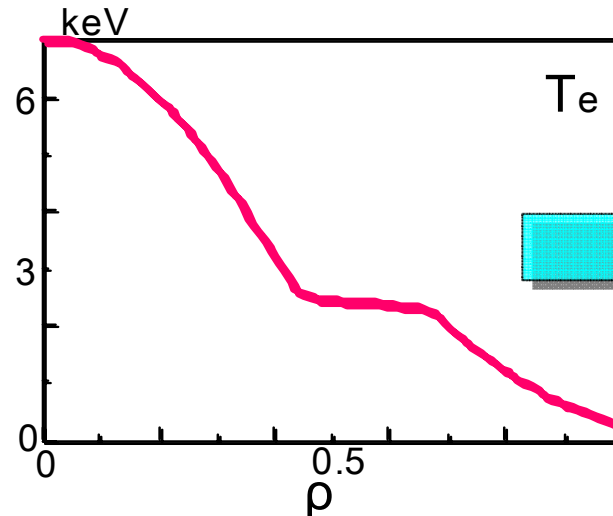
Degradation model in TOPICS

Flattening effect model:
Amplified diffusivities is enlarged inside island

χ in island (ρ) = $C(\rho) \cdot \chi(\rho)$

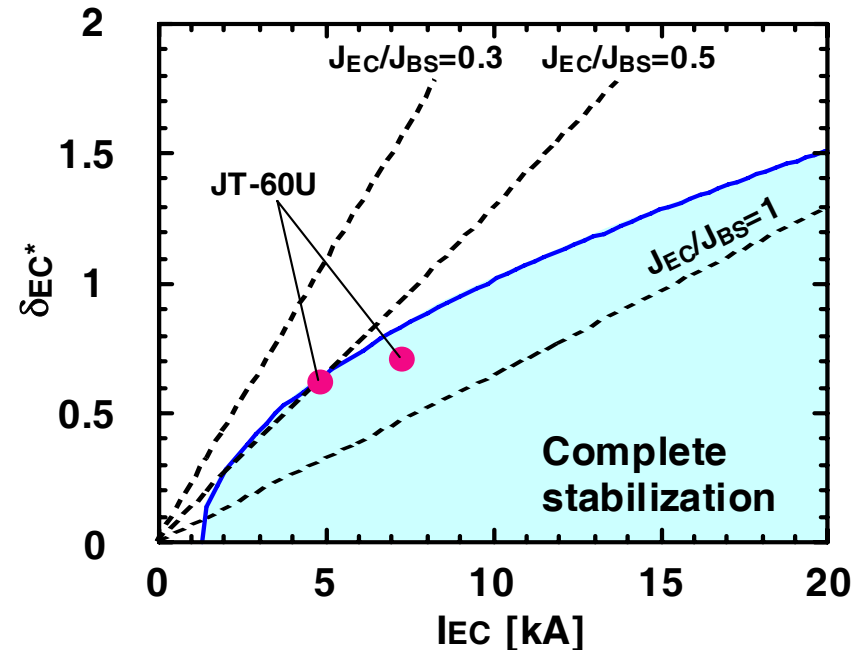
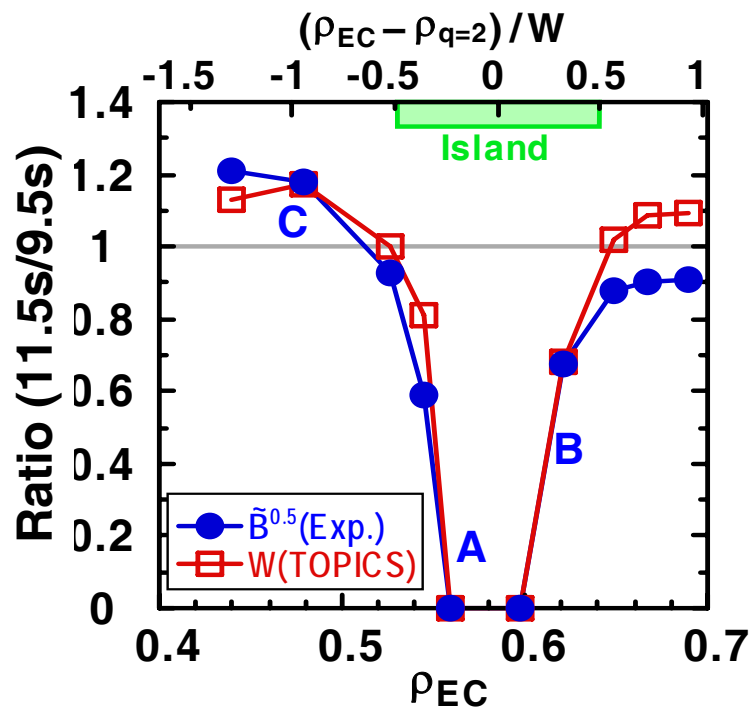
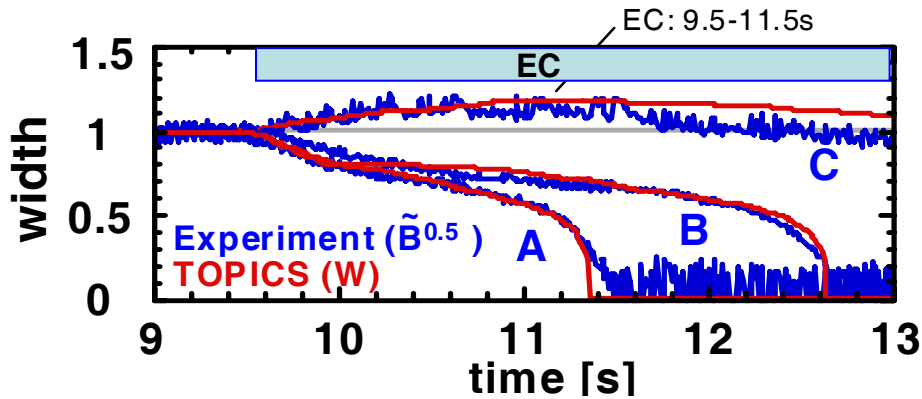
$$C(\rho) = 1 + C_0 \left\{ 1 - \left(\frac{\rho - \rho_s}{W/2} \right)^2 \right\}^2$$

$$C_0 = \text{Min} \left[20, 10^4 (W - W_{init})^3 \right]$$



NTM simulation with modified Rutherford equation was verified by experimental results.

Integrated modelling in JAEA



- Good agreement with the same coefficient set

- The consistent analysis shows:**
- ECCD width has stronger effect than amount of EC-driven current.
 - Precise ECCD control has enabled complete stabilization with smaller value of j_{EC}/j_{BS} :

$$J_{EC}/J_{BS} \sim 0.5$$

[A. Isayama, IAEA FEC 2006]



Ideal MHD stability model

mainly with N.Aiba, S.Tokuda

collaboration with

M. S. Chu¹⁾, P. B. Snyder¹⁾, and H. R. Wilson²⁾

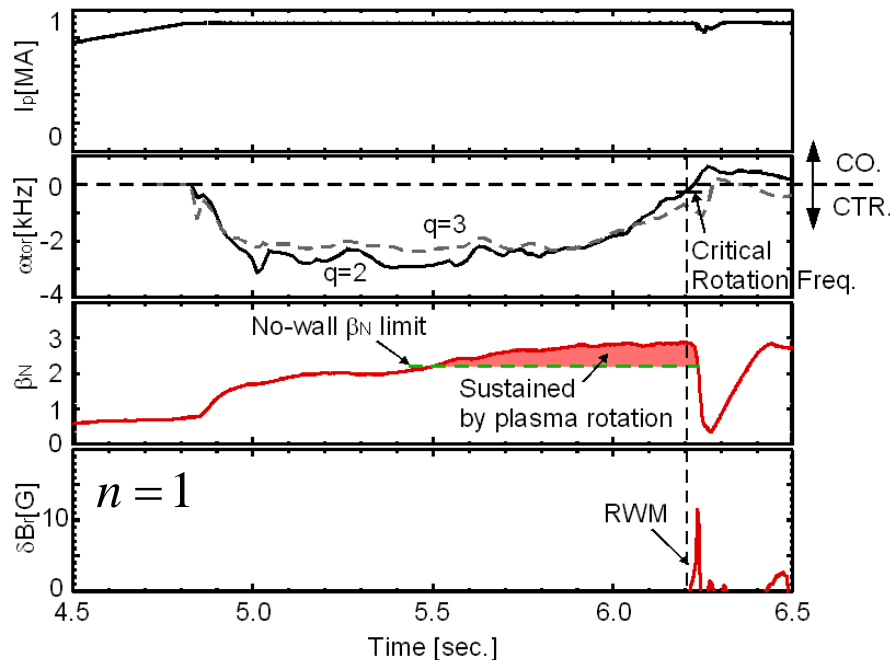
1) General Atomics, 2) Univ. York

Background

Integrated modelling in JAEA

In tokamaks, ideal MHD modes often limit plasma performance.

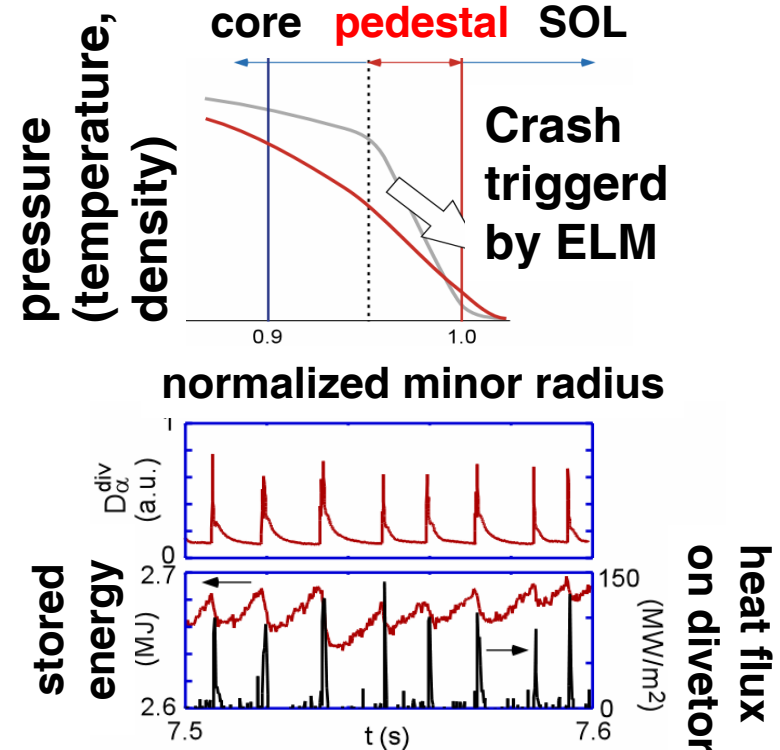
**Kink-Ballooning Mode
(Beta limits, related to RWM)**



G.Matsunaga in this meeting 01aA03P.

**Triggered by a global
(low- n) MHD mode.**

**Edge Localized Mode (ELM)
(Peeling-Ballooning Mode)**



ELM experimental results in JT-60U

**Triggered by an edge
localized (intermediate to
high- n) MHD mode.**

Ideal MHD stability codes

Integrated modelling in JAEA

MHD spectrum codes have been developed for the linear stability analysis of ideal MHD modes.

1. For the low- n mode stability analysis
... ERATO^[1], DCON^[2], MISHKA^[3] etc.
2. For the intermediate to high- n mode stability analysis
... ELITE^[4,5], MISHKA etc.

These codes have succeeded to analyze the stability of these MHD modes and are used for experimental analyses.

In JAEA, the MHD spectrum code **MARG2D** has been developed for a fast stability analysis of wide n range of ideal MHD modes^[6,7].

[1] R. Gruber et al, Comput. Phys. Commun 21, 323 (1981).

[2] A.H.Glasser et al. in Bull. Am. Phys. Soc. vol.42, 1848 (1997).

[3] A.B.Mikhailovskii et. Al., Plasma Phys. Rep. 23, 844 (1997).

[4] H.R.Wilson et. al., Phys. Plasmas 9, 1277 (2002).

[5] P. B. Snyder et al., Phys. Plasmas 9, 2037 (2002).

[6] S Tokuda et al, J. Plasma Fusion Res. 73, 1141 (1997).

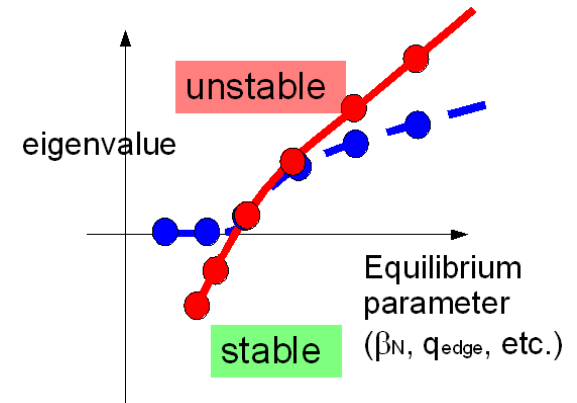
[7] N. Aiba et al., Comput. Phys. Commun. 175, 269 (2006).

Overview of the MARG2D code

Integrated modelling in JAEA

With conventional ideal MHD model, the stability boundary of ideal MHD modes cannot be revealed explicitly in tokamaks.

MARG2D can identify explicitly the stability boundary of ideal MHD modes by solving the eigenvalue problem associated with the 2-D Newcomb equation with FEM^[5].



$$N\mathbf{Y} = -\lambda R\mathbf{Y}, \quad (\mathbf{Y} = r\xi_r)$$

$$R_{l,m} \propto \begin{cases} (m/q - n)^2 & \dots l = m \\ 0 & \dots l \neq m \end{cases}$$

N : Newcomb operator

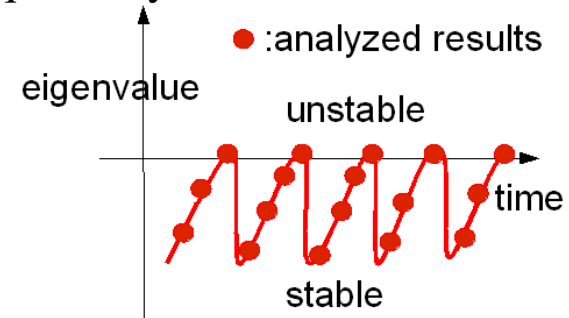
ξ_r : displacement in the r direction

m : poloidal mode number

n : toroidal mode number

q : safety factor

This is a fruitful advantage for the integrated simulation code: TOPICS-IB.



Computing the growth rate by adopting the plasma inertia

Integrated modelling in JAEA

In the physical model introduced, since the physical inertia term is changed artificially, the linear growth rate γ of unstable ideal MHD mode cannot be estimated.



Turn back the plasma inertia and the boundary condition at the rational surfaces after identifying the plasma is unstable.

$$RY \Rightarrow \rho(\mathbf{Y} + (\mathbf{V} - \beta\mathbf{Y}))$$

$$\lambda \Rightarrow \gamma$$

\mathbf{V} : displacement vector in the $\nabla\psi \times \mathbf{B}$ direction

ρ : plasma density

β : unorthogonality of the coordinate

This realizes to estimate γ with the incompressible assumption.

Benchmarking results between the MARG2D code and

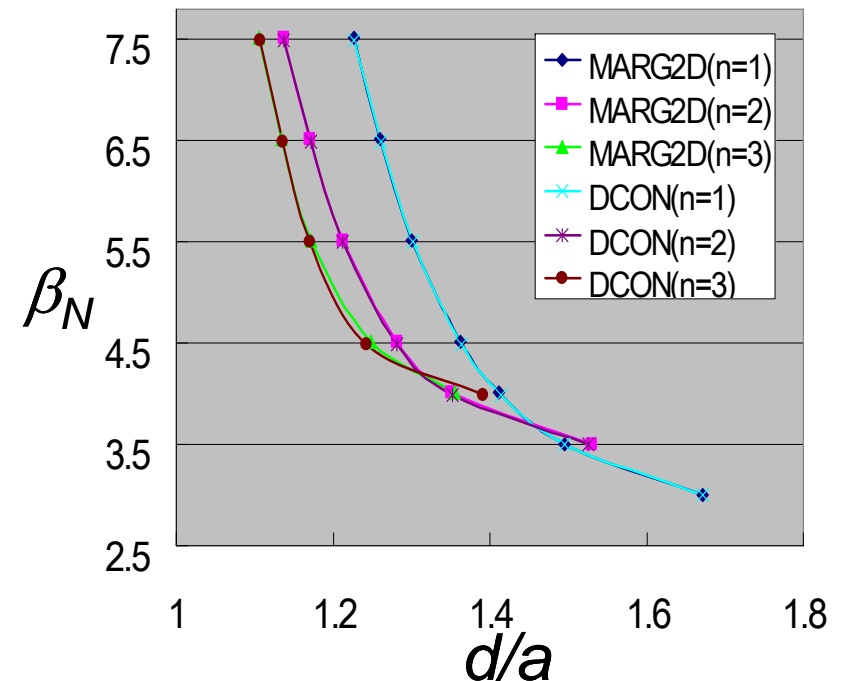
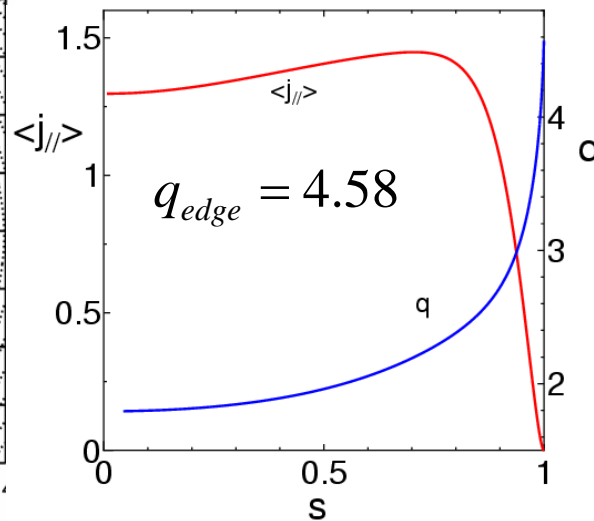
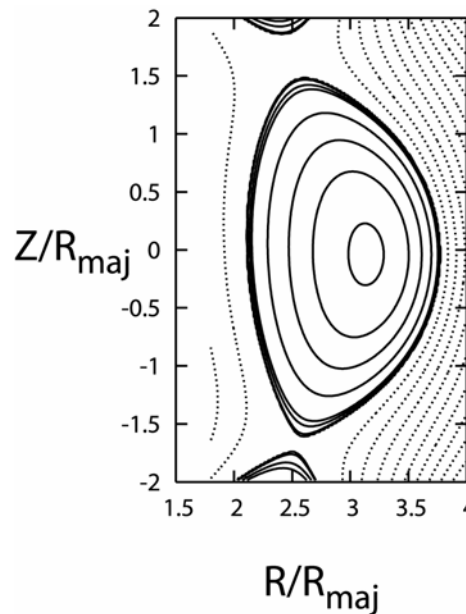
Integrated modelling in JAEA

- 1. the DCON code** by low- n external MHD modes stability analysis.
(collaborated with Dr. M. S. Chu)
- 2. the ELITE code** by intermediate to high- n external modes stability analysis.
(collaborated with Dr. P. B. Snyder and Dr. H. R. Wilson)

Benchmarking results 1 (low- n mode case)

Integrated modelling in JAEA

- DCON solves the 2-D Newcomb equation with the shooting method^[2].
- The wall position (d/a) dependence of the β_N limit determined by the external kink-ballooning mode stability as the benchmark test. (The shape of the outermost surface and q_{edge} are fixed.)



Both codes shows the almost the same β_N limit determined by the MHD stabilities whose $n=1, 2,$ and 3 .

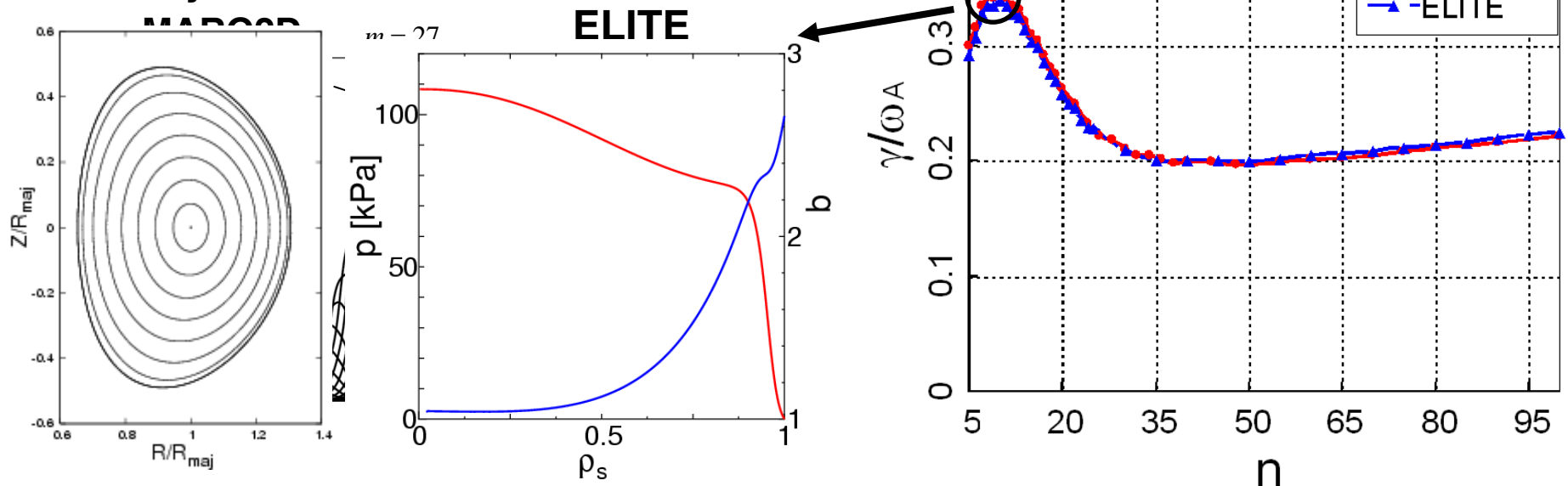
Benchmarking result 2

(intermediate to high- n mode case)

Integrated modelling in JAEA

ELITE code solves the eigenvalue problem associated with the ideal MHD equation simplified with the high- n ordering (keep multiple orders for the intermediate and high- n mode analysis)^[4,5].

Eigenfunction of the most unstable mode ($n=10$) is analyzed with MARG2D and ELITE.



- In the range $5 \leq n \leq 100$, the growth rates (γ/ω_A) obtained by ELITE and MARG2D are well identical to each other.
- The structure of the eigenfunction is also almost same as each other.

Integrated Modelling in JAEA



Integrated ELM model

mainly with N.Hayashi, T.Takizuka, N.Aiba

Integrated edge-pedestal model

Integrated modelling in JAEA

1.5D core transport code (TOPICS)

1D transport & current diffusion equations
2D Grad-Shafranov equation

[N. Hayashi, IAEA
FEC 2006]

2D MHD
equilibrium

**ELM model :
Enhance transport**

Heat & particle
flows across
separatrix

Boundary
conditions at
separatrix

Eigenvalue & Eigenfunction

Linear MHD stability code (MARG2D)

Eigenvalue problem of 2D
Newcomb equation
Applicable to wide range of
mode numbers from low to high

SOL-divertor model (Five-point model)

Flux-tube geometry
Integral fluid equations
Exponential radial profiles with
characteristic scale length

SOL model (Hayashi, PSI06)

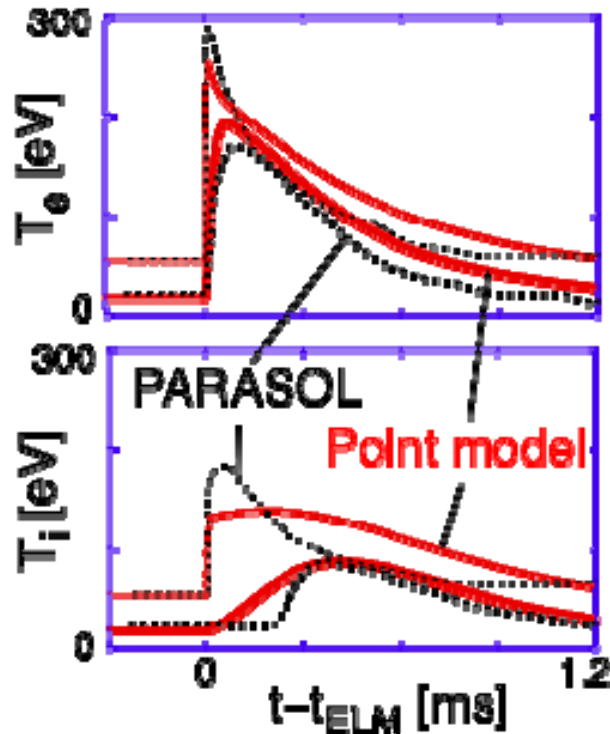
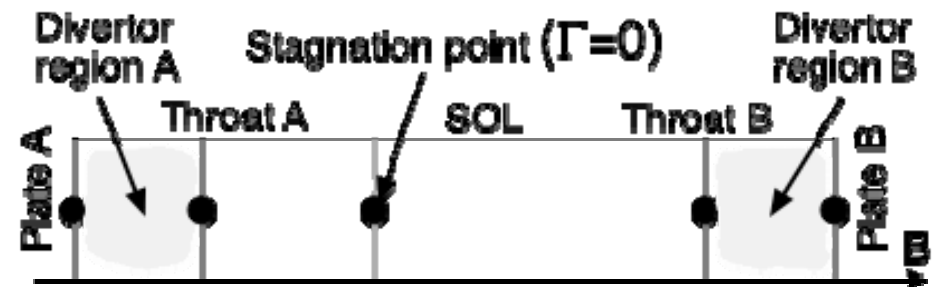
Integrated modelling in JAEA

Point model based on integral fluid equations easily reproduces many static features found in experiments. (Stangeby, textbook)

Dynamic version of the point model (Five-point model) has been developed for the integrated ELM modeling.

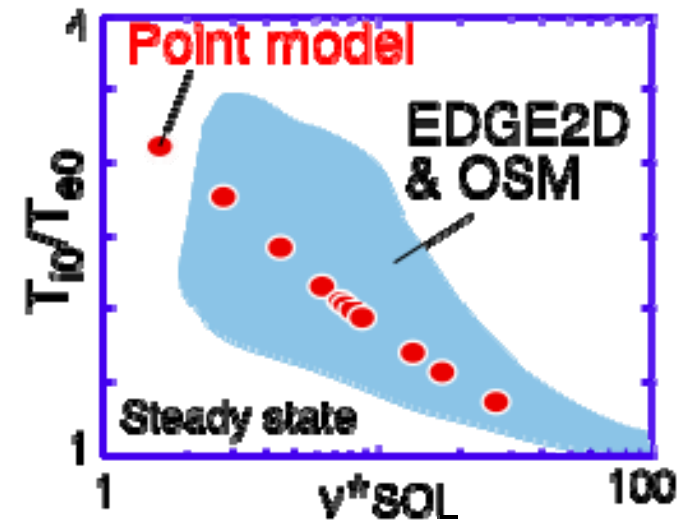
Flux-tube geometry

- 2 SOL & 2 divertor regions(5 positions)
- Symmetry assumed in this paper



Validated by particle code

Validated by fluid codes

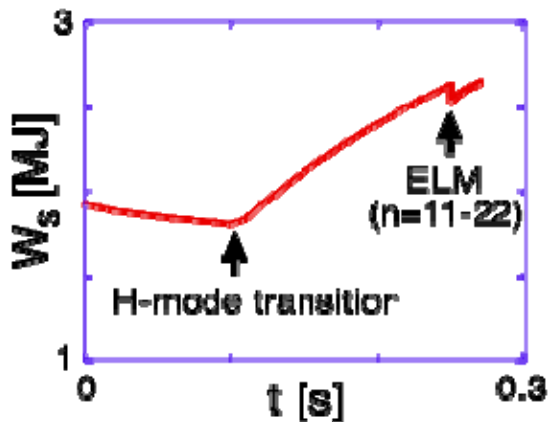
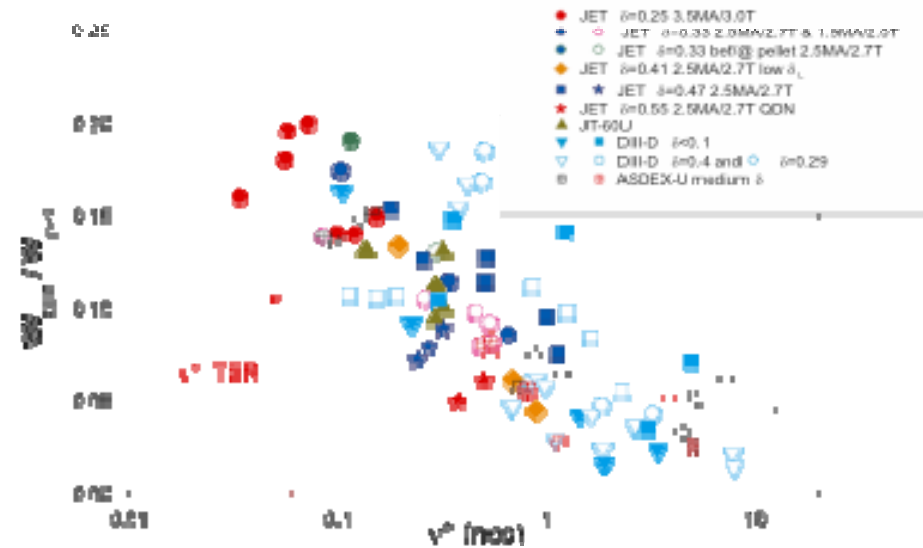


Parallel heat conduction and equipartition energy depend on the collisionality.

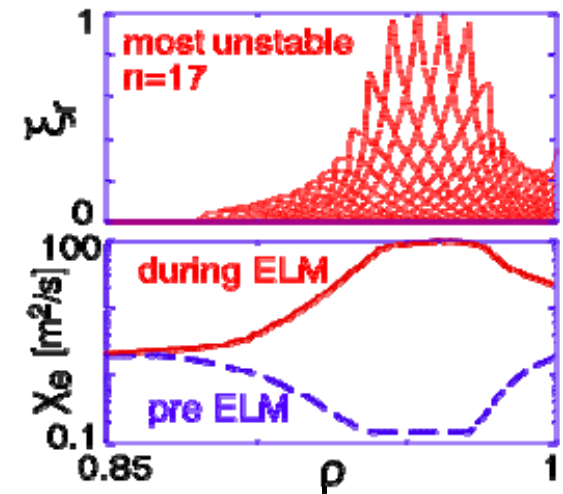
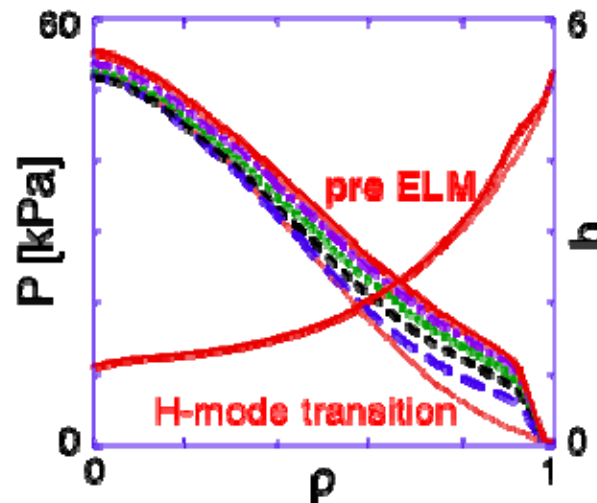
ELM energy loss simulation

Integrated modelling in JT-60U

- Energy loss by ELMs is crucial for reducing the divertor plate lifetime and limiting the plasma confinement.
- ELM energy loss was found to decrease with increasing the collisionality in multi-machine experiments.
- The collisionality dependence is investigated.
- ELM phenomena is simulated in JT-60 parameters.



Pedestal formation : Neoclassical transport in peripheral region and anomalous in inside region.



Stabilities of n=1-30 modes are examined in each time step.

Transient behavior of core-pedestal-SOL-divertor plasmas along pedestal growth and ELM crash

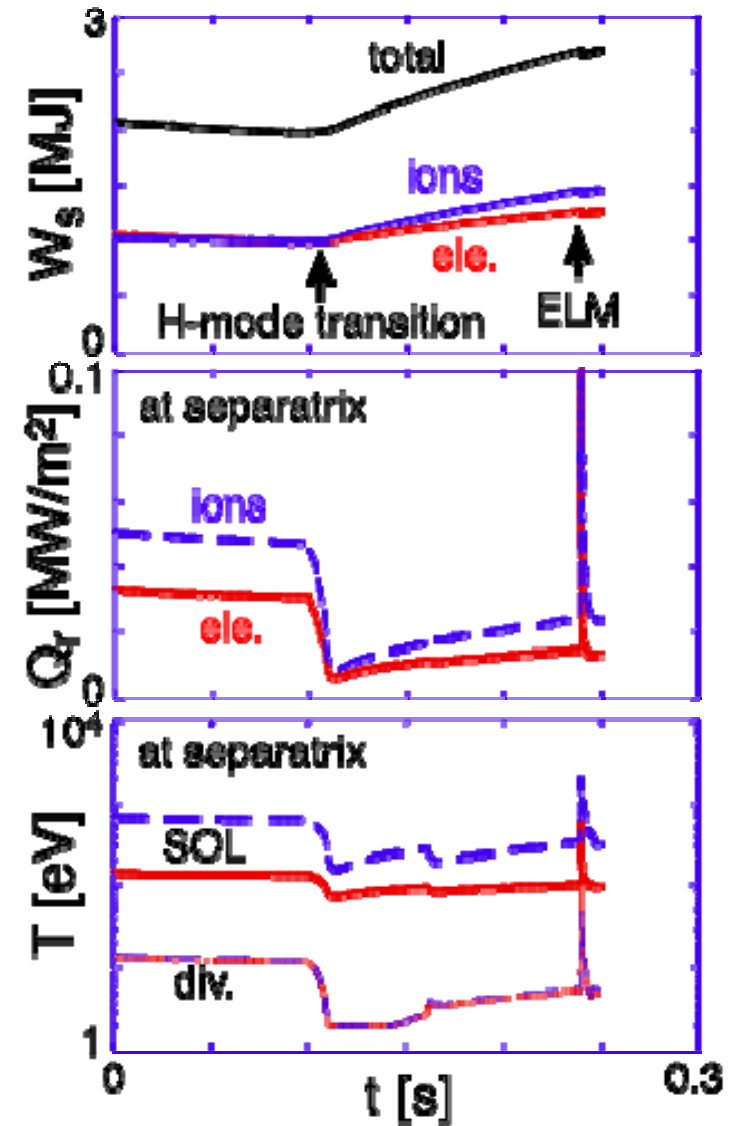
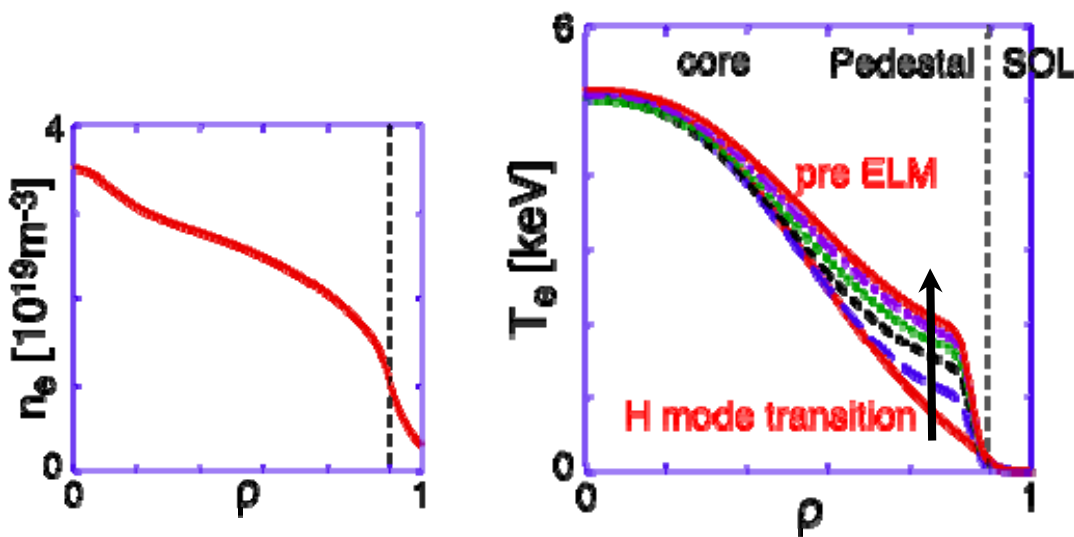
Integrated modelling in JAEA

Simulation condition : JT-60U like parameters

- $R=3.4$ m, $a=0.9$ m, $I_p=1.5$ MA, $B_t=3.5$ T, $\kappa\sim 1.5$, $\delta\sim 0.21$,
 $Z_{\text{eff}}=2.3-2.8$, $P_{\text{NB}}=12$ MW, $\beta_N=0.8-1$

- ELM duration $\delta t_{\text{ELM}} = 200$ μs , diffusivity $\chi_{\text{ELM}}^{\text{max}}=100$ m^2/s , Pedestal width $\Delta_{\text{PED}} = 0.05$

- Fixed density profile,
 $n_{\text{div}}=1 \times 10^{20}$ m^{-3} (High recycling divertor)



Increase of SOL temperature mitigates the radial edge gradient and lowers the ELM energy loss.

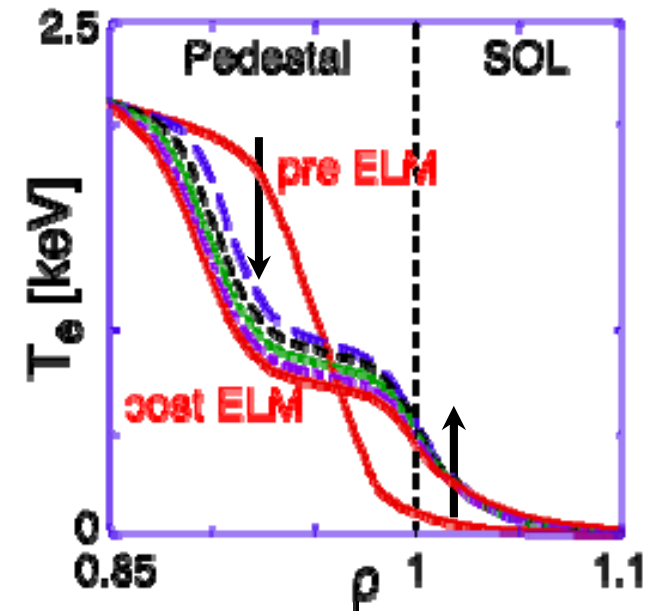
Integrated modelling in JAEA

Energy flows into the SOL and the SOL-divertor temperatures rapidly increases.

The resultant energy loss ($< 10\%$ of W_{ped}) is comparable with that in JT-60U.

Electron energy loss is larger than the ion one, due to larger heat conduction parallel to the magnetic field.

By the integration of the SOL model, the consistent analysis was obtained.

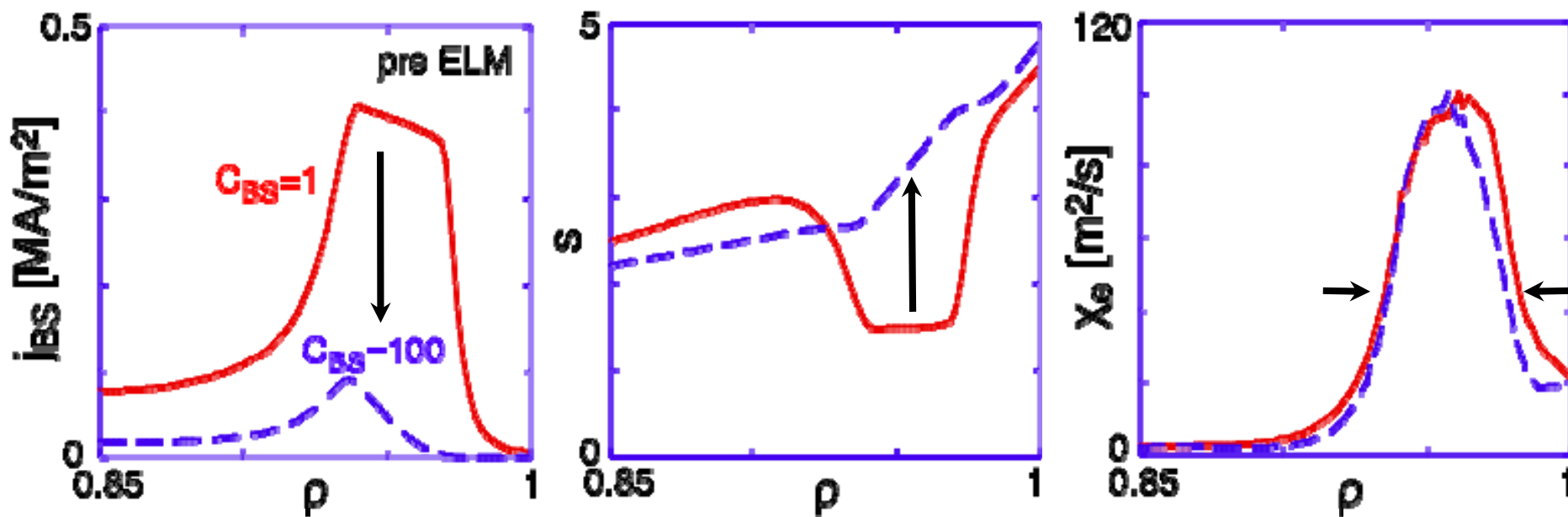


a) Bootstrap current effect

The collisionality in the bootstrap current model is artificially enhanced by $C_{BS}=100$ (enhanced collisionality: $v^*_{ped} = C_{BS} v^*_{ped0} = 9$).

Bootstrap current decreases with increasing the collisionality and intensifies the magnetic shear at the pedestal region.

The increase of magnetic shear reduces the width of eigenfunctions of unstable modes.

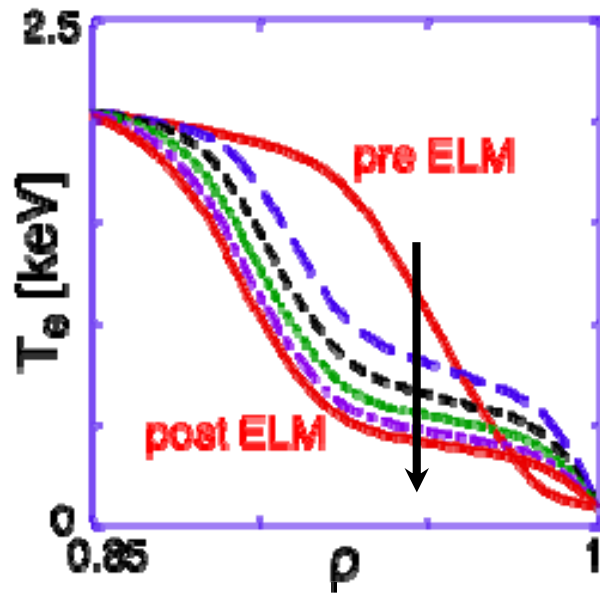


ELM energy loss is reduced by increasing collisionality in bootstrap current.

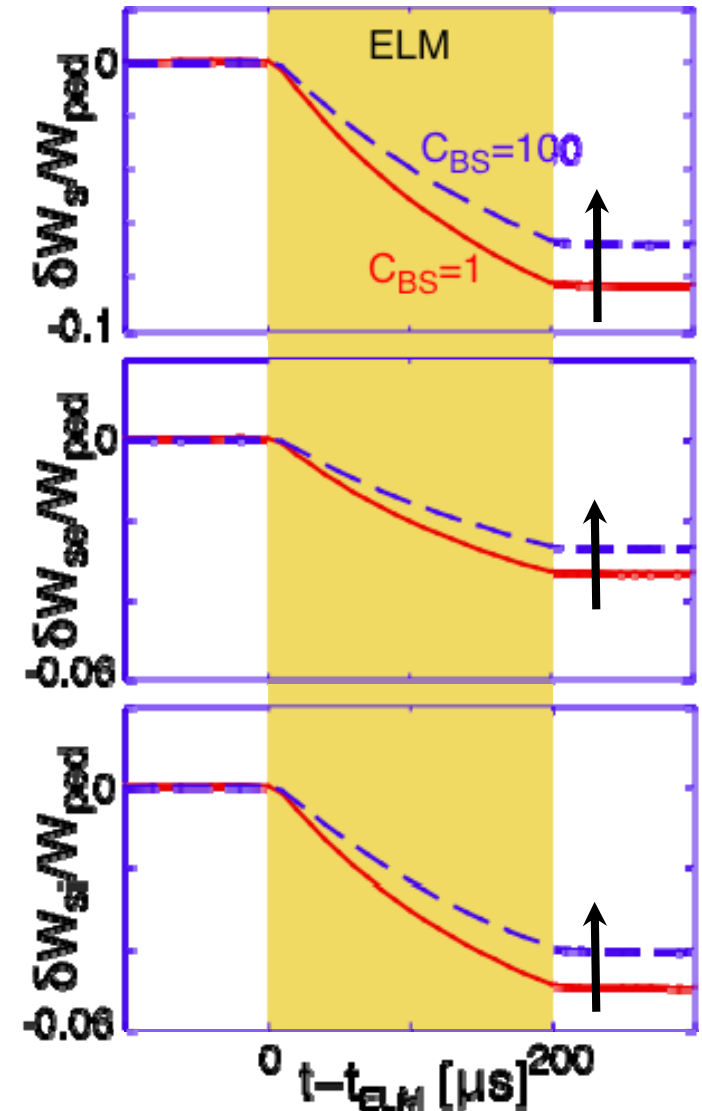
Integrated modelling in JAEA

Simulation condition : $T_{\text{SOL}}=100$ eV, SOL model is not used to clear only the bootstrap current effect.

Both electron and ion energy losses are reduced in almost the same ratio.



fixed B.C.
w/o SOL model



b) SOL transport effects

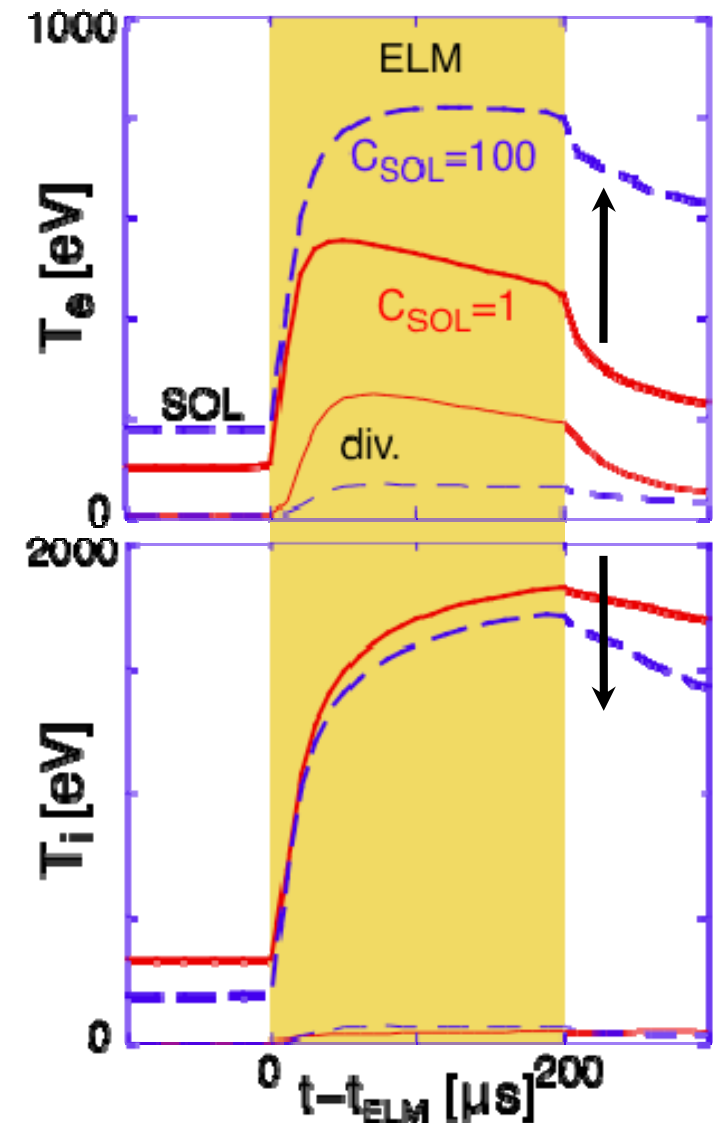
Integrated modelling in JAEA

The collisionality in SOL model is artificially enhanced by $C_{\text{SOL}}=100$ ($v_{\text{ped}}^*=9$).

SOL electron temperature increases with the collisionality, because the parallel heat conduction is inversely proportional to the collisionality.

SOL ion temperature decreases with increasing the collisionality, because the equipartition energy flows is proportional to the collisionality.

SOL electron temperature increases with collisionality, while ion one decreases.



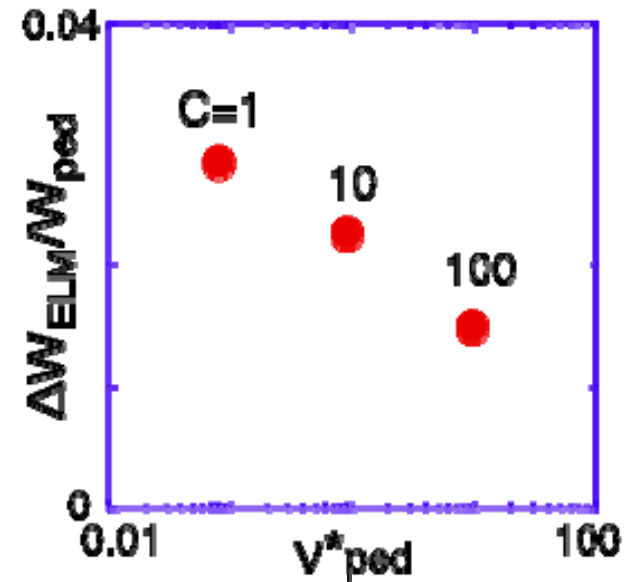
c) Both effects of bootstrap current and SOL transport on ELM energy loss

Integrated modelling in JAEA

Collisionality in both models is enhanced by $C=C_{BS}=C_{SOL}$.
When the collisionality is enhanced by $C=100$,
the electron energy loss is reduced by about 1/3,
but the ion one is reduced a little.

Total energy loss is reduced about half.

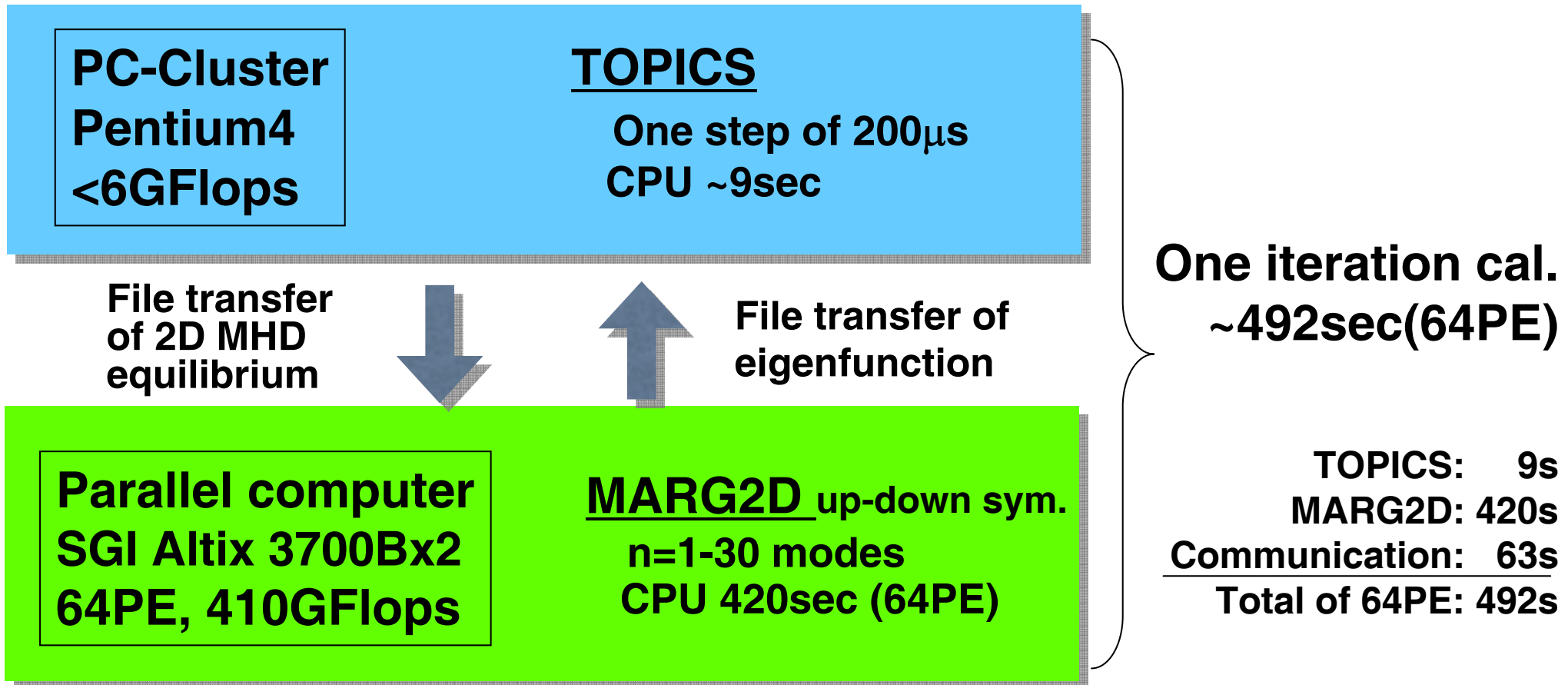
By the above two mechanisms, the ELM energy loss decreases with increasing the collisionality. The bootstrap current and the SOL transport have the **major effect on the collisionality dependence**.



Value of $\Delta W_{ELM}/W_{ped} \sim 0.05$ was measured in JT-60U plasmas with $v^*_{ped} \sim 0.1$.

Computer system and calculation time on Integrated calculation of ELM

Integrated modelling in JAEA



- Estimated cal. time is 136.7hours (5.7days) for 200msec simulation for 200 μ s iteration, using 64PE.

3. Summary

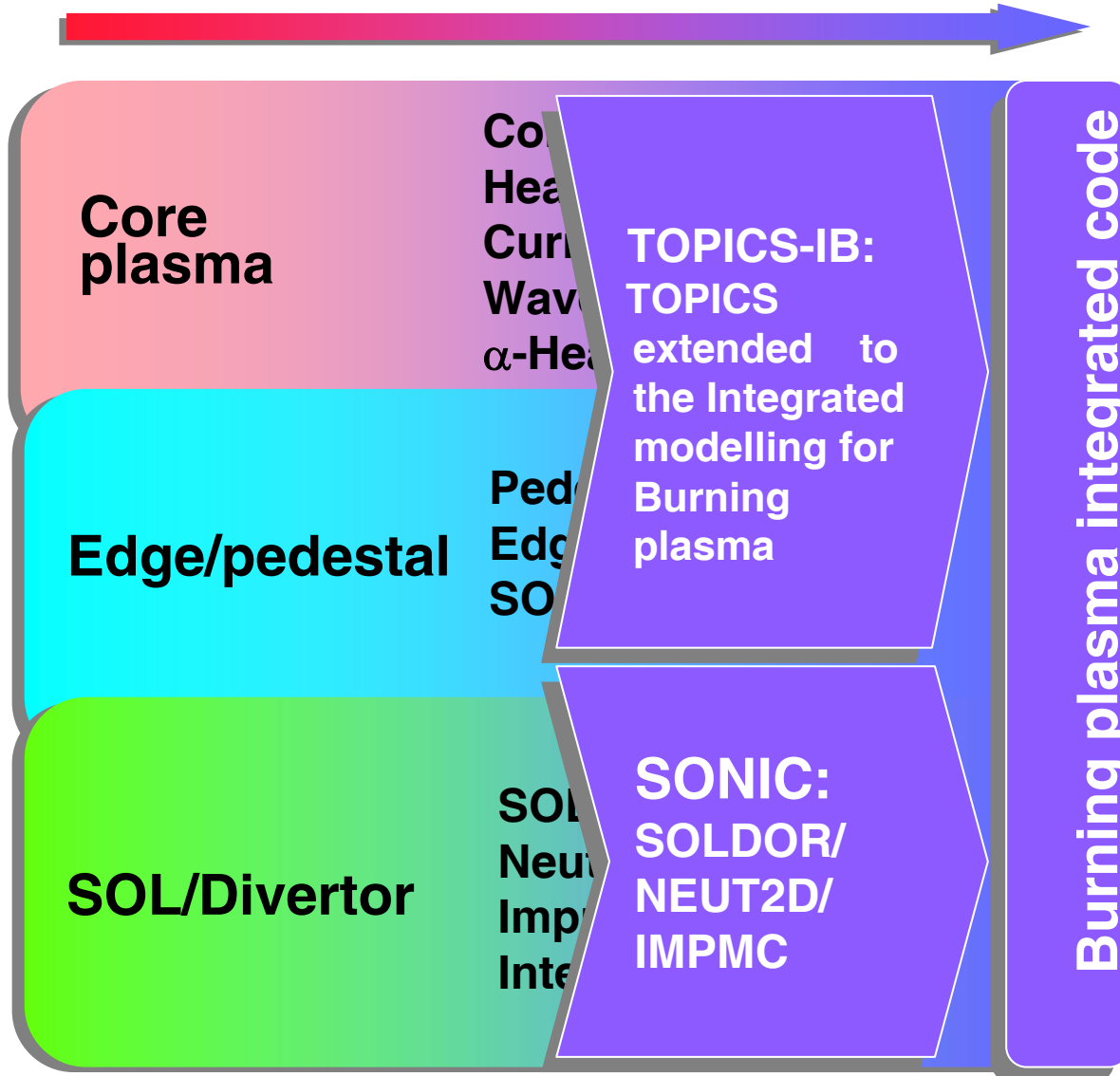
Integrated code TOPICS-IB has been developed, presented here, based on the 1.5D transport code with the MHD stability model.

- ✓ NTM model has been developed with the integration of the transport code, the ECCD code and the modified Rutherford equation. Stabilizing effects of NTM by ECCD were clarified by the consistent analysis. Optimization of EC profile was obtained.
- ✓ The ideal MHD stability code MARG2D has been developed for the low and high n stability with a short CPU time.
- ✓ Using the MARG2D as the ELM mode, the integrated model of the pedestal-ELM-SOL has been developed.
- ✓ The Integrated model has been clarified self-consistent effects of ELM energy loss on the collisionality.

Consistent analysis by the integrated code are useful to investigated the complex plasma and control the integrated performance.

Plan for integration of whole plasma

Integrated modelling in JT-60U



Two ways for whole plasma simulation of burning plasma

- 1) TOPICS-IB will extend to the divertor region:**
 - Dynamic response
 - Simple divertor model
 - Transport model is key
- 2) SONIC will extend to the core region:**
 - Accurate divertor model
 - 2D transport model

The construction of integrated model according the purpose of research is important.

Integrated Modelling in JAEA



Appendix

Background

Integrated modelling in JAEA

- **Burning plasma has very wide time and spatial scales, and complex physics such as Turbulence, Transport, MHD, Wave-particle interaction, Plasma-wall interaction, Atomic and molecular physics**
- **Control of complex plasmas is the big issue:**
 - **High confinement, High beta, High bootstrap, High radiation, Suppression of impurity, α -heating dominant**
 - **Strong coupling of pressure, current and momentum profiles**
 - **Control of autonomous plasmas**
 - **Control of the burning of the fusion reaction**

To solve these issues:

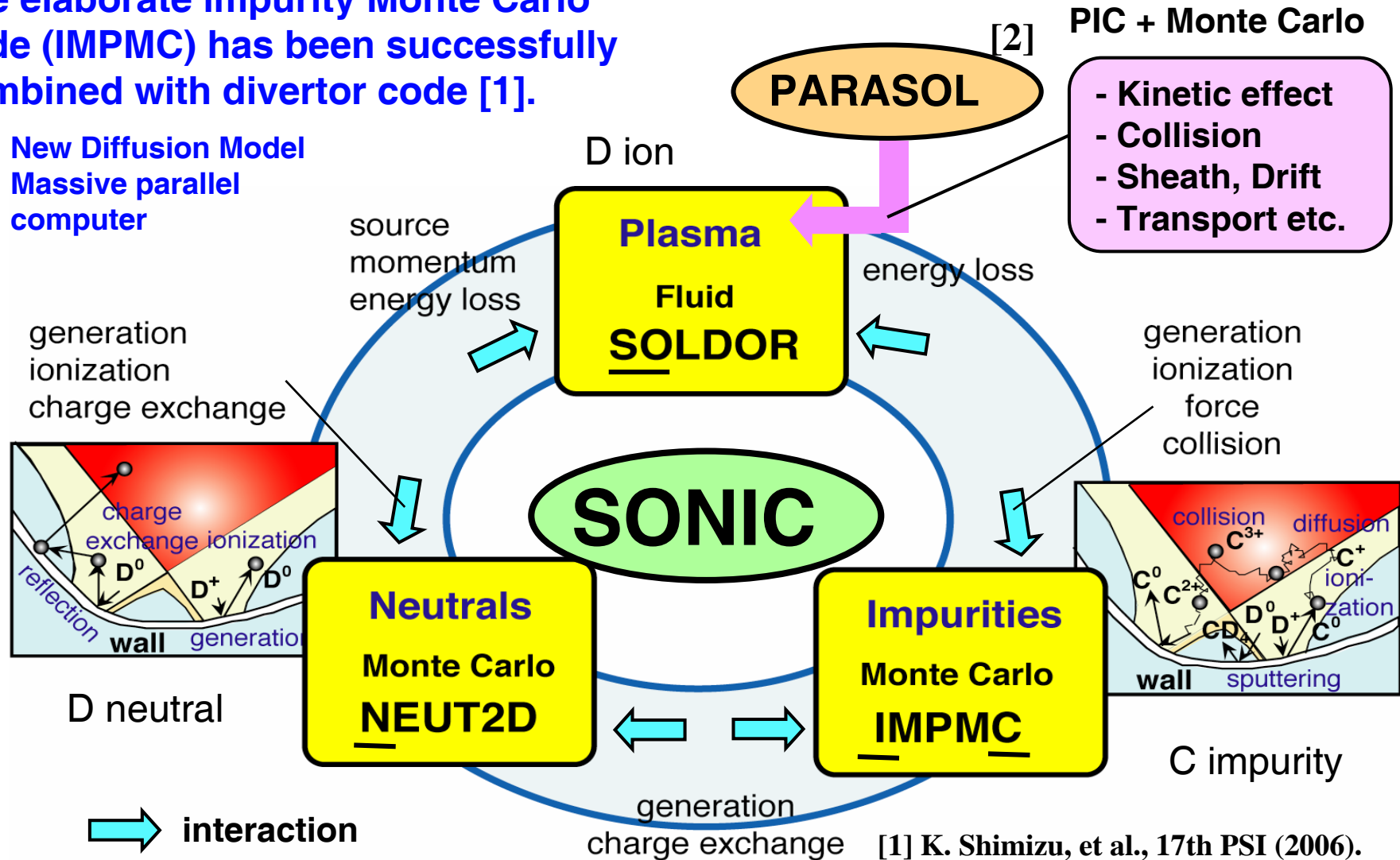
- **It is not realistic to simulate the whole burning plasma based on the first principle at the present.**
- **Modeling and integration of the model are a useful method for the complex burning plasma.**

Integrated SOL-divertor code:SONIC

Integrated modelling in JT-60U

The elaborate impurity Monte Carlo code (IMP MC) has been successfully combined with divertor code [1].

- New Diffusion Model
- Massive parallel computer



[1] K. Shimizu, et al., 17th PSI (2006).

[2] T. Takizuka, et al., 15th PSI (2002).

Plasma Potential Energy of the Ideal MHD Model (Background2)

Integrated modelling in JAEA

On the basis of the ideal MHD model, the plasma potential energy can be expressed as

$$W_p = \frac{1}{2} \int \int \int \left[\frac{1}{\mu_0} |\mathbf{Q}_\perp|^2 + \frac{1}{\mu_0} \left| Q_{\parallel} \mathbf{b} - \mu_0 \frac{\xi \cdot \nabla p}{B^2} \mathbf{B} \right|^2 + \Gamma p |\nabla \cdot \xi|^2 \right]$$

$$- \frac{\mathbf{j} \cdot \mathbf{B}}{B^2} (\xi \times \mathbf{B}) \cdot \mathbf{Q} - 2(\xi \cdot \nabla p)(\xi \cdot \kappa) \sqrt{g} d\tau,$$

$$\mathbf{Q} := \mathbf{Q}_\perp + Q_{\parallel} \mathbf{b} = \nabla \times (\xi \times \mathbf{B}), \quad \kappa := (\mathbf{b} \cdot \nabla) \mathbf{b}.$$

- The first, second, and third terms are the stabilizing terms called **the Shear Alfvén term**, **the Compressional Alfvén term**, and **the sound wave term**, respectively.
- The third and fourth terms are the destabilizing terms driven by **the parallel current** and **the pressure gradient**.
- **A kink-ballooning mode and a peeling-ballooning mode are destabilized by the coupling of both current and pressure terms.**

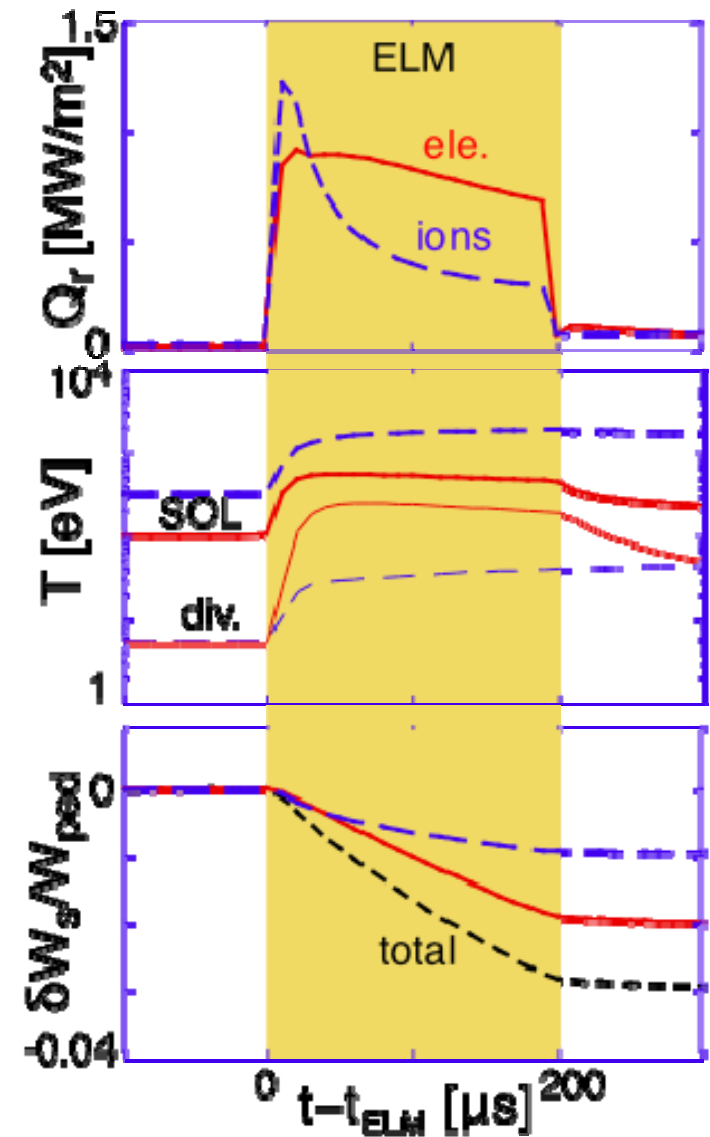
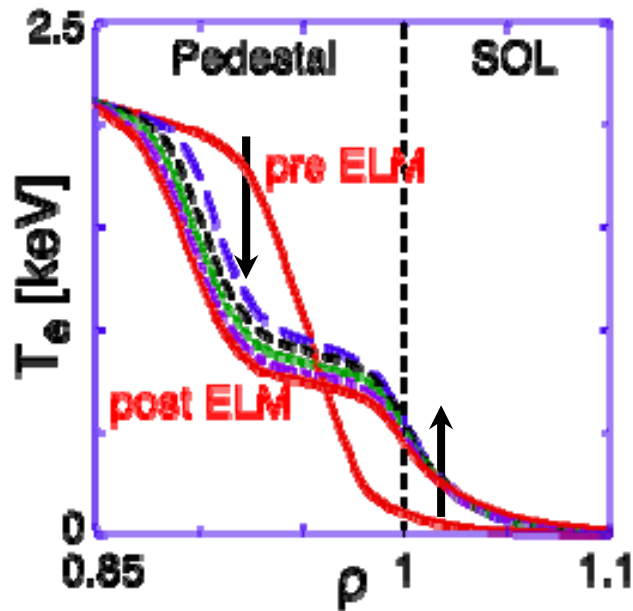
Increase of SOL temperature mitigates the radial edge gradient and lowers the ELM energy loss.

Integrated modelling in JAEA

Energy flows into the SOL and the SOL-divertor temperatures rapidly increases.

The resultant energy loss ($< 10\%$ of W_{ped}) is comparable with that in JT-60U.

Electron energy loss is larger than the ion one, due to larger heat conduction parallel to the magnetic field.



ELM energy loss is reduced by increasing collisionality in SOL transport.

Integrated modelling in JAEA

For higher collisionality, the SOL electron temperature increases more and the electron energy loss is reduced.

On the contrary, the SOL ion temperature decreases and the ion energy loss is enhanced a little.

Total ELM energy loss is reduced according to the electron energy loss and the ion contribution is small.

